

Gelaste, niet-verplaatsbare, drukloze tanks van thermoplasten.
Deel 3: Constructie en berekening van enkelwandige rechthoekige tanks

Publicatie uitsluitend voor commentaar

Welded static non-pressurized thermoplastic tanks.
Part 3: Design and calculation for single skin rectangular tanks

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Commentaar voor 1 februari 1997

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prEN 12573-3 Welded static non-pressurized thermoplastic tanks. Part 3: Design and calculation for single skin rectangular tanks

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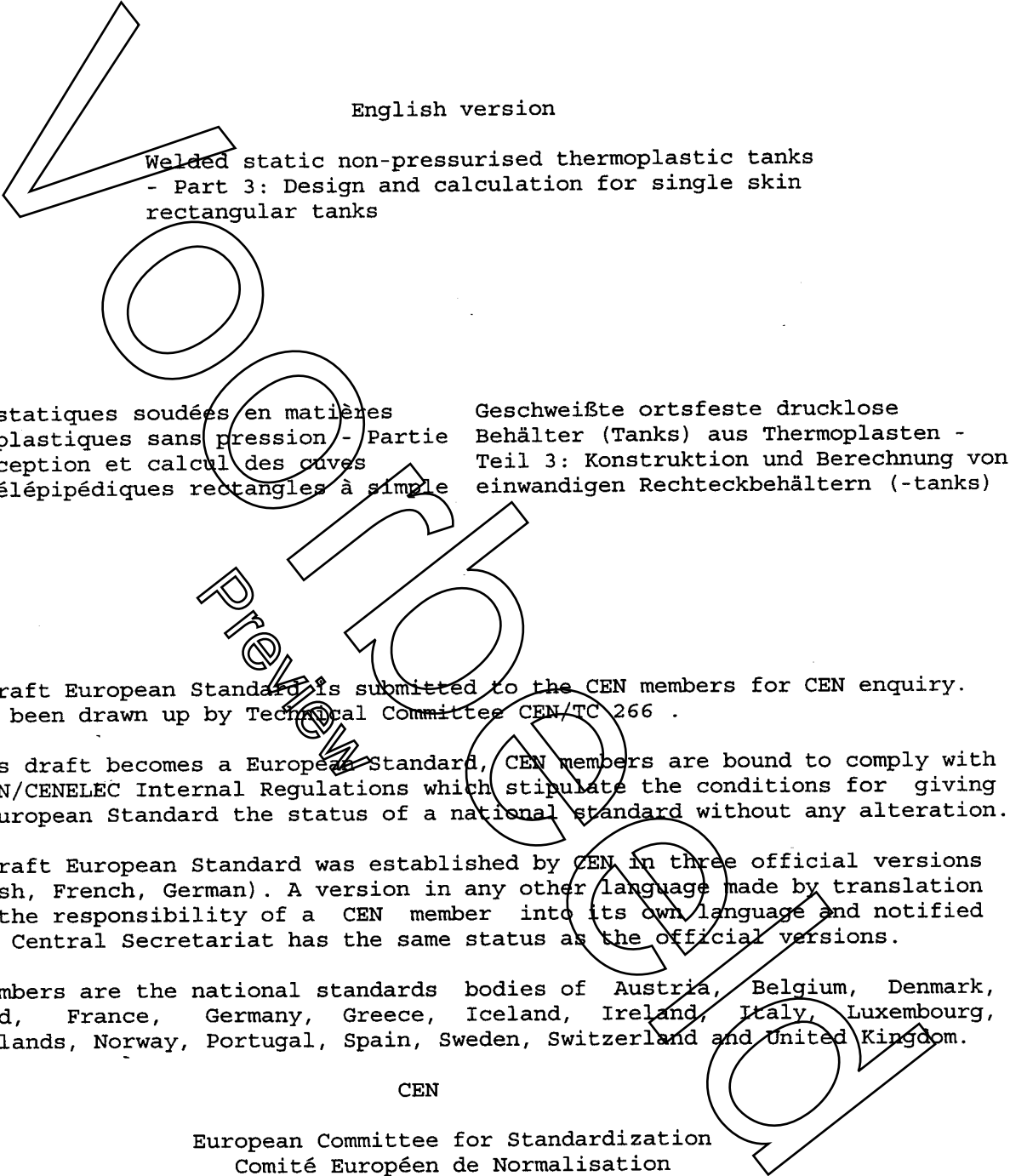
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- Part 3: Design and calculation for single skin
rectangular tanks

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Behälter (Tanks) aus Thermoplasten -
Teil 3: Konstruktion und Berechnung von
einwandigen Rechteckbehältern (-tanks)

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It has been drawn up by Technical Committee CEN/TC 266 .

If this draft becomes a European Standard, CEN members are bound to comply with
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Contents

	Page
Foreword	4
1 Scope	4
2 Normative references	4
3 Definitions, symbols and abbreviations	5
3.1 Definitions	5
3.2 Symbols and abbreviations	5
4 General considerations in design calculations	5
5 Unstiffened tanks sitting on a continuous flat rigid surface	7
5.1 General	7
5.2 Aspect ratio $x/y < 0,5$	7
5.3 Aspect ratio $0,5 \leq x/y \leq 4$	8
5.4 Aspect ratio $x/y > 4$	8
6 Tanks with rim stiffening supported on a continuous flat rigid surface	8
6.1 Calculation of the skin thickness	8
6.1.1 General	8
6.1.2 Aspect ratio $x/y < 0,5$	9
6.1.3 Aspect ratio $0,5 \leq x/y \leq 2$	9
6.1.4 Aspect ratio $x/y > 2$	9
6.2 Calculation of rim stiffeners	10
7 Tanks with intermediate horizontal stiffeners supported on a continuous flat rigid surface	11
7.1 General	11
7.2 Calculation of the minimum skin thickness	11
7.2.1 General	11
7.2.2 Calculation for the top panel	11
7.2.3 Calculation for the intermediate and bottom panels	12
7.2.3.1 General	12
7.2.3.2 Aspect ratio $x/y < 0,5$	12
7.2.3.3 Aspect ratio $0,5 \leq x/y \leq 2$	12
7.2.3.4 Aspect ratio $x/y > 2$	12
7.3 Calculation of the horizontal stiffeners	12
8 Tank with cross-ribbed horizontal and vertical stiffeners supported on a continuous rigid surface	13
8.1 Calculation of the minimum skin thickness, base thickness and horizontal stiffeners	13
8.2 Calculation of the vertical stiffeners	13
9 Rectangular tank with U-frame	14
9.1 General	14
9.2 Calculation of the skin thickness of the side walls	15
9.3 Determination of the tank base	15
9.3.1 Aspect ratio $x/z < 0,5$	15
9.3.2 Aspect ratio $0,5 \leq x/z \leq 2$	15
9.3.3 Aspect ratio $x/z > 2$	15
9.4 Calculation of the vertical stiffeners	15

10	Determination of the size of the tank cover	16
10.1	General	16
10.2	Freely supported tank cover	16
10.3	Fixed cover	16
10.3.1	General	16
10.3.2	Aspect ratio $1 \leq x/z \leq 2$	16
10.3.3	Aspect ratio $x/z > 2$	17
10.4	Stiffened tank cover	17
10.4.1	Calculation of the skin thickness and deflection	17
10.4.2	Determination of the size of stiffeners used with a tank cover	17
11	Special cases	18
11.1	Intermittently supported tanks	18
11.2	Limits of validity for the plate theory design method	18
11.2.1	General	18
11.2.2	Rigidity $N \leq 30$	18
11.2.3	Rigidity $N > 30$	19
11.2.4	Rigidity $N > 1000$	19
Annex A (informative)	Construction details of rectangular tanks	
Annex B (informative)	Bibliography	

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Foreword

This European Draft Standard has been prepared by CEN/TC 266 "Thermoplastic static tanks", the secretariat of which is held by BSI.

The Technical Committee CEN/TC 266 decided to submit this European Draft Standard to the CEN-enquiry.

The informative annex A gives some construction details of rectangular tanks as examples.

The informative annex B is a bibliography.

This European Standard consists of 4 parts:

Welded static non-pressurised thermoplastic tanks;

- Part 1: General principles
- Part 2: Calculation of vertical cylindrical tanks
- Part 3: Design and calculation of single skin rectangular tanks
- Part 4: Design and calculation of flanged joints

1 Scope

This part of European Standard specifies the design and calculation for single skin rectangular tanks, fabricated from the following thermoplastics:

- Polyethylene (PE)
- Polypropylene (PP)
- Poly (vinyl chloride) (PVC)
- Poly (vinylidene fluoride) (PVDF)

The tanks may be strengthened on the outside by means of ribs or frames made of the same or other materials, such as glass-fibre reinforced plastic (GRP) or steel.

Tanks which comply with the requirements of this standard are not intended to withstand internal pressure or vacuum, other than that which may occur during the transfer of fluids (including gases) in their normal operation. The precise figures that apply are given in part 1 of this standard.

Plate theory was used as the basis of the calculation in this document. Reference to membrane theory is found in 11.2.

2 Normative references

This European Standard incorporates by dated or undated reference, provisions from other publications. These normative references are cited at the appropriate places in the text and the publications are listed hereafter. For dated references, subsequent amendments to or revisions of any of these publications apply to this European Standard only when incorporated in it by amendment or revision. For undated references the latest edition of the publication referred to applies.

- EN XXXX-1 Welded static non-pressurised thermoplastic tanks – Part 1: General principles
- EN 1778 Characteristic values for welded thermoplastic constructions – Determination of allowable stresses and moduli for design of thermoplastic equipment

3 Definitions, symbols and abbreviations

For the purposes of this part of this European Standard the following definitions, symbols and abbreviations apply:

3.1 Definitions

Skin: Basic structural element of the tank.

Stiffener: Section attached horizontally or vertically to the skin of the tank.

Wall: Skin of the tank plus stiffeners.

Panel: Area of the skin between stiffeners.

U-frame: Stiffener running beneath the base and vertically up the side of the tank.

3.2 Symbols and abbreviations

E	is the elastic modulus of the stiffener material (with plastics, this corresponds to E_c), in N/mm^2
$E_{c(al),D}$	is the allowable creep modulus at the design condition for deformation (temperature, stress, time, medium), in N/mm^2 , see prEN 1778
F	is the force, in N
f	is the maximum deflection, in mm
J	is the moment of inertia of stiffener, in mm^4
k	is the correction coefficient
M	is the bending moment, in Nmm
p	is the excess pressure on the tank base, in N/mm^2
p_m	is the mean value of excess pressure for calculation of skin thickness, in N/mm^2
p_1	is the mean value of excess pressure for calculation of the stiffener, in N/mm^2
t	is the skin thickness, in mm
W	is the moment of resistance of rim stiffeners, in mm^3
x	is the length of the tank or distance between the vertical stiffeners, in mm
x'	is the effective length of panels assigned to stiffeners, in mm
y	is the depth of the tank or distance between the horizontal stiffeners, in mm
y'	is the effective depth of panels assigned to stiffeners, in mm
z	is the width of the panel or panel, in mm
$\alpha_1 \dots \alpha_5$	is the deformation coefficient
$\beta_1 \dots \beta_5$	is the skin thickness coefficient
σ_{al}	is the allowable stress, in N/mm^2 , see prEN 1778

4 General considerations in design calculations

Calculation methods are only given for the tank designs illustrated in figures 1 to 5.

Welds shall be situated in regions of low bending moments; the maximum moments are shown in figures 6, 7 and 8.

NOTE: The design should take account of the effects of thermal expansion between the tank wall and any external stiffening.

For construction details of rectangular tank see annex A.

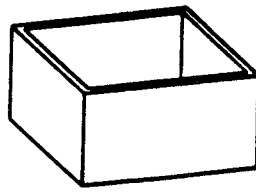


Figure 1: Unstiffened tank

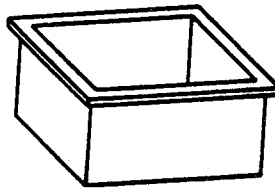


Figure 2: Tank with a horizontal rim stiffener

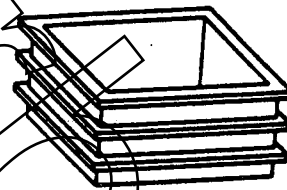


Figure 3: Tank with intermediate horizontal stiffeners

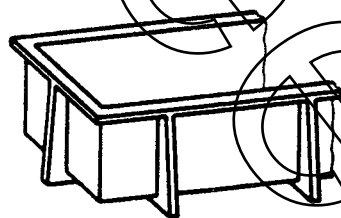


Figure 4: Tank with vertical stiffeners

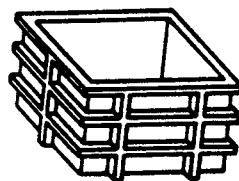


Figure 5: Tank with cross-ribbed horizontal and vertical stiffeners

5 Unstiffened tanks sitting on a continuous flat rigid surface

5.1 General

The calculation of the minimum skin thickness depends on the ratio between the length (x) and depth (y) (see figure 6). The thickness of the base shall be of similar magnitude to the actual thickness of the skin.

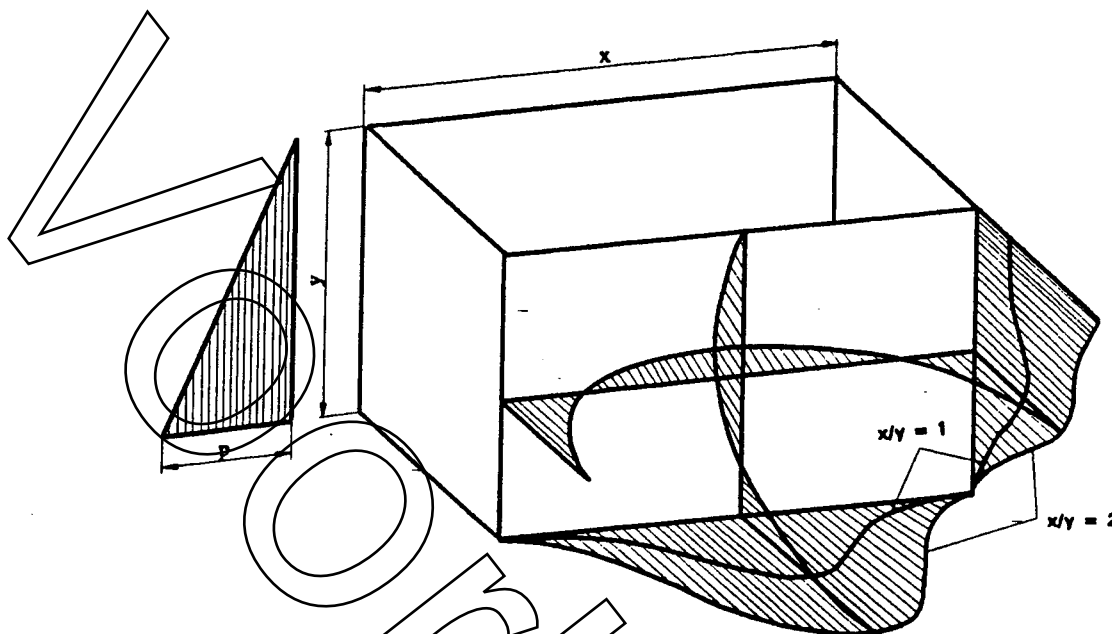


Figure 6: Distribution of bending moments

5.2 Aspect ratio $x/y < 0,5$

The minimum skin thickness shall be calculated according to equation (1).

$$t = \sqrt{\frac{p \cdot x^2}{2,5 \sigma_{al}}} \quad (1)$$

NOTE 1: In equation (1) for the skin thickness (t), the skin has been assumed as a beam fixed at both ends with the load distributed uniformly between these two points. This leads to a factor of 2 in the denominator. To provide better agreement with measured values, the factor was increased to 2,5.

The maximum deflection of the skin shall be calculated according to equation (2).

$$f = \frac{p \cdot x^4}{32 \cdot k \cdot E_{c(al),b} \cdot t^3} \quad (2)$$

The factor k is either 1 when $x < y$ or 2 when $x/y \approx 0,5$.

NOTE 2: In equation (2) for the deflection, there is a factor of 32 in the denominator when a beam is fixed at both ends with the load distributed uniformly between these two points. However, it is possible to use equations based on plate theory which exactly correspond to the particular load case and lead to a factor of 68 if $x/y \approx 0,5$. Therefore, an additional factor k was introduced, which, depending on x/y , gives sufficiently accurate results.

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